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<b>(21) International Application Number:</b> PCT/EP96/01063 <b>(22) International Filing Date:</b> 13 March 1996 (13.03.96) <b>(30) Priority Data:</b> 9505153.8      14 March 1995 (14.03.95)      GB <b>(71) Applicant (for all designated States except US):</b> ROCKWOOL INTERNATIONAL A/S [DK/DK]; 501 Hovedgaden, DK-2640 Hedehusene (DK). <b>(72) Inventors; and</b> <b>(75) Inventors/Applicants (for US only):</b> JENSEN, Soren, Lund [DK/DK]; Rudesovej 11, DK-2840 Holte (DK). CHRIS-TENSEN, Vermund, Rust [DK/DK]; Soager 11, St. Valby, DK-4000 Roskilde (DK). JENSEN, Leif, Moller [DK/DK]; Moseager 5, St. Valby, DK-4000 Roskilde (DK). <b>(74) Agent:</b> GILL JENNINGS & EVERY; Broadgate House, 7 Eldon Street, London EC2M 7LH (GB).		<b>(81) Designated States:</b> AL, AM, AT, AU, AZ, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IS, JP, KE, KG, KP, KR, KZ, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, US, UZ, VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).  <b>Published</b> <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
<b>(54) Title:</b> METHOD OF MAKING MINERAL FIBRES  <b>(57) Abstract</b>  <p>The invention provides a method for making MMV fibres from a charge which comprises a mixture of at least two types of briquettes. The overall chemical analysis of the briquette mixture gives initial melting temperature (I) when provided in the form of a single type of briquette. This single type of briquette also gives compression strength (i) over the operating temperature range 1,200 °C to 1,340 °C. The briquette mixture charged to the furnace is such that at least 30 wt.% of the charge is in the form of briquette which have IMT at least 20 °C greater than IMT (I) and/or is such that at least 30 wt.% of the charge comprises briquettes having compression strength over the working temperature range greater than compression strength (i) at each temperature.</p>		

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### METHOD OF MAKING MINERAL FIBRES

This invention relates to methods for the production of mineral fibre materials. In particular it is useful in the production of mineral fibres having content of phosphorus, boron or alkali metal.

It is well known to provide man-made vitreous fibres (MMVF) by a process comprising melting in a furnace a charge comprising suitable raw materials to form a melt and forming fibres from the melt. The raw materials may comprise mineral materials in the form of finely ground or coarse particulate material. Recently it has become known to provide mineral materials in the form of moulded briquettes of particulate mineral material. Briquettes are a convenient form in which to charge mineral materials, in particular those which tend to be available in fine particulate form.

Generally when briquettes are used it is standard practice to provide a single type of briquette only, that is to provide all briquettes with the same chemical analysis. When certain materials such as phosphorus and boron are included in the charge it is generally convenient to provide a high proportion of the total charge in briquette form, for instance three quarters or substantially all of the charge. In particular, we believe that increasing need in the future for careful control of the chemical analysis of the melt will lead to increasing use of briquettes as a means of providing most or nearly all of the required mineral materials for the charge.

Once it is decided that briquettes are to carry a large proportion of the required mineral components into the melt it becomes necessary for the briquettes to have a complex chemical analysis. This is particularly the case for melts intended to produce fibre compositions which have become desirable of late, for instance those containing phosphorus and/or boron and/or alkali metals. In briquettes containing a large number of chemical components, there is a high risk of eutectics being formed

between groups of chemical components which result in lowering the melting temperature of the briquette. Some materials or combinations of materials can induce phase separation in the melt.

5       The quality of the fibres produced is influenced by the quality of the melt exiting the furnace for formation into fibres. To obtain high quality fibres it is important to achieve a regular flow of melt from the furnace at controlled or constant viscosity and temperature. In  
10       particular it is important that the melt which exits the furnace is at a suitably high temperature.

      It is particularly important to minimise pressure variations in the furnace and to control the temperature of the melt, in particular to minimise the pressure decrease  
15       over the melting zone, in order to permit maintenance of controlled conditions.

      In a cupola furnace the melting process is strongly influenced by the flow of air from the tuyeres at the bottom of the furnace through the charge to the exhaust at  
20       the top of the furnace. This air flow is highly dependent upon the amount of free space between the coke and the mineral materials making up the charge. In a cupola furnace the air flow is disrupted when the amount of this  
25       space becomes too low. In such a situation the pressure drop across the charge increases, as do pressure variations. This results in variations in the flow of melt through the furnace outlet onto the fibre-forming equipment.

      To avoid this situation it is important that the raw  
30       materials are able to retain adequate resistance to compression (compression strength) at furnace temperatures. If compression strength is reduced at a rather low furnace temperature (for instance around 1,200°C) the raw materials become compressed by further materials entering the furnace  
35       above them and the free space between the materials is reduced. Compression strength at furnace temperatures is related to the melting point (and in particular the initial

melting point) of a particular component. Compression strength of a briquette is reduced when parts of it begin to melt, so lower melting point materials will tend to have a lower compression strength at a given temperature than  
5 higher melting point materials.

Therefore the creation of low melting eutectics and consequent reduction in the melting temperature of briquettes making up a substantial proportion of the charge can lead to a serious reduction in compression strength.  
10 This results in the charge becoming compressed and reduces the potential air flow space, disrupting air flow and pressure control. If the charge materials melt too rapidly the charge may tend to collapse. The melt then becomes viscous and the melt exiting the furnace is inhomogeneous  
15 and has too low a temperature.

It would be desirable to be able to provide the complex compositions which are now particularly commercially desirable without disrupting melting and air flow, in particular in cupola furnaces. It would also be  
20 particularly desirable to be able to achieve this without sacrificing the convenience and benefits of using briquettes as a means of providing charge materials.

In the invention we overcome the problems of the prior art by splitting the component of the charge which is  
25 provided in the form of briquettes. We thus provide at least two types of briquette in the charge and can ensure that a sufficient proportion of the charge is in briquettes which have melting point suitably high to support the remainder of the charge, even if some of the remainder has  
30 very low melting point and low resistance to compression.

According to the invention there is provided a method of making MMV fibres comprising melting in a furnace raw materials to produce a mineral melt and forming fibres from  
35 the melt,

in which the raw material charge includes a mixture of at least two types of briquette (a) and (b), of size at

least 50 mm, each type of briquette having a different chemical analysis, and at least 30 wt% of the raw material charge is provided by briquettes (b)

and in which either

5 (1) briquette (a) has an initial melting temperature of 1,240°C or below and briquette (b) has an initial melting temperature of 1,200°C or greater and the initial melting temperature of briquette (b) is at least 20°C greater than the initial melting temperature of briquette  
10 (a),

or

(2) the briquettes have an overall chemical analysis which when provided in the form of a single type of briquette gives an initial melting temperature (I), and in  
15 which briquettes (b) have an initial melting temperature which is at least 20°C greater than initial melting temperature (I).

Often, briquettes comply with both definition (1) and definition (2).

20 We find that by use of the invention it is possible to provide the briquette component of a charge in the form of briquettes of at least two types and thus to ensure that at least 30% of the charge has melting temperature high enough to avoid the melt and air flow problems discussed above.  
25 Thus this proportion of the charge can support other components and prevent the charge from collapsing. This is achieved at the same time as providing an overall briquette chemical analysis which could lead to formation of eutectics and low melting point if the entire  
30 composition were present in a single briquette. Thus complex chemical analyses for melts can be achieved in the invention whilst retaining the convenience of providing a significant proportion of the charge in the form of briquettes.

35 In this specification the initial melting temperature (IMT) is measured by differential thermal analysis (DTA). This well-established method is described by Paul D. Garn

in "Thermoanalytical Methods of Investigation", Academic Press, 1965, pp 16-52. The briquettes used in the method of the invention are a mixture of several mineral materials and consequently do not in general melt at a single temperature but over a range of temperatures. For the purposes of the commercially used melting process it is the temperature at which melting begins which is particularly important. This is the initial melting temperature, which is defined as the temperature at which the first endotherm peak occurs.

IMT is measured as follows:

Materials are provided in the same proportions as those in the briquette to be analysed. These materials are ground or crushed to a particle size of below 100  $\mu\text{m}$ . The ground or crushed material is mixed to ensure it is homogeneous. A 50 mg sample is used for the DTA experiment, which is carried out using a heating rate of 10°C/minute.

In the method of the invention "briquettes" are bodies formed by agglomeration of particulate mineral material, which have a compression strength sufficient to enable the briquettes to be transported. The process of forming briquettes of particulate mineral material generally comprises the steps of addition to the particulate mineral materials of a suitable binder, mixing, compacting/shaping and curing etc to achieve the required quality.

In the invention the briquettes generally have a size of at least 50 mm. The "size" of a component as used in the specification is the maximum sieve hole size through which not more than 10% of the component will pass. That is, a material having a size of at least 50 mm is such that at least 90% by weight of the material is retained on a sieve having holes of size of 50 mm. Preferably the briquettes have a size of at least 80 mm. Preferably at least 90% by weight of the briquettes pass through a sieve of hole size 300 mm, more preferably 250 mm, most preferably 200 mm, and in particular 160 mm.

In the invention, the briquette component of the charge comprises a mixture of at least two types of briquette. A "type" of briquette is one which has a specified chemical analysis. Different types of briquettes will have different chemical analyses. Briquettes of the same type may be produced from different basic materials, provided that the final chemical analysis of the briquette as a whole is the same. It is however preferred that all briquettes of the same type are made up from the same set of raw materials.

In the invention the briquettes (b) have high melting point in comparison with other components of the charge or in comparison with the melting point which would be exhibited by the overall briquette composition. These high melting briquettes (b) provide at least 30 wt% of the total charge, preferably at least 50 wt%.

In the invention the briquettes (b) can be provided so as to have an IMT of at least 1,200°C and in combination with briquettes (a) which have IMT of 1,240°C or below, the IMT of briquettes (b) being at least 20°C greater than the IMT of briquettes (a).

Therefore the charge comprises briquettes (a) which melt at a low temperature and have a tendency to be compressed. Briquettes (b) melt at a higher temperature and thus travel further down the furnace whilst retaining their structure. This facilitates retention of adequate interstices between the raw materials and the coke and enables the air to flow evenly from the tuyeres to the exhaust through the charge.

Briquettes (a) always have IMT below 1,240°C. Usually this is below 1,220°C, more generally below 1,200°C, often below 1,190°C. Briquettes having IMTs at the lower temperatures (1,200°C and below) will tend to lead to air flow problems and consequent melt flow problems in almost all furnaces. Combination of these briquettes with briquettes (b) generally alleviates these problems.



Briquettes (b) always have an initial melting temperature above 1,200°C and at least 20°C greater than the IMT of briquettes (a). In certain furnaces, and where the IMT of component (a) is particularly low, an IMT of component (b) of 1,200°C or greater, more often 1,220°C or greater gives adequate results. Generally however the IMT of component (b) is 1,240°C or greater, preferably 1,250°C or greater, more preferably 1,260°C or greater.

Preferably briquettes (b) have IMT at least 30 or 40°C greater than the IMT of component (a).

Alternatively, in the invention splitting of the briquettes may be based on the IMT (I) of a single briquette formed from a composition having the chemical analysis of the overall briquette composition. The invention is particularly useful where IMT (I) is 1,240°C or below, preferably 1,220°C or below. Particular benefits are seen when the overall chemical analysis would give an IMT (I) of 1,200°C or below, in particular 1,190°C or below.

In this aspect, the mixture of briquettes gives an overall chemical analysis which has its own IMT (I) if present in a single briquette.

At least two types of briquette must be present. Three, four or even five types of briquette or more may be included. Preferably however not more than three types, and in particular only two types of briquette are included in the charge.

The mixture of briquettes is such that they comprise briquettes (b), which make up at least 30 wt%, usually at least 50 wt%, of the total charge, and which have an IMT increased relative to IMT (I). They have IMT at least 20°C above IMT (I). Preferably the increased IMT is at least 30°C, more preferably at least 40°C, above IMT (I).

The fraction (b) having this required IMT can comprise briquettes of various different IMT's. It can also comprise briquettes of different types having the same IMT.

Preferably however in the process the briquettes are such that those having the same IMT are all of the same type.

The briquettes (b) of IMT increased relative to IMT (I) provide at least 30 wt%, preferably at least 50 wt% and  
5 more preferably at least 75 wt% of the total briquettes.

It is preferred that at least 50 wt% of the total briquettes have IMT 1,200°C or greater, preferably 1,220°C or greater, more preferably 1,240°C or greater. IMT may be as high as 1,250°C or greater, and even above 1,260°C.

10 It is permissible for some briquettes, for instance up to 70 wt% of the briquettes, to have IMT below IMT (I). Preferably however 40 wt% or less, more preferably 20 wt% or less, most preferably 10 wt% or less of the briquettes have IMT below IMT (I). It is possible for substantially  
15 none of the briquettes to have IMT below IMT (I).

Preferably no briquettes have IMT more than 30°C, more preferably more than 20°C, most preferably more than 10°C, below IMT (I). In particular, the lower the IMT of the briquettes the more desirable it is for the proportion of  
20 these in the charge to be low.

It is also permissible to include in the charge some briquettes which have IMT the same as IMT (I). Preferably not more than 40 wt%, more preferably not more than 20 wt%, more preferably not more than 10 wt% of the briquettes,  
25 have this IMT. In particular it is preferred that substantially zero briquettes have this IMT.

In general it is preferred that the at least two types of briquette are such that they all have IMT above IMT (I), that is the amount of briquettes (a) is substantially zero.  
30 If there are at least two types of briquette having IMT above IMT (I), then preferably the difference between their IMT's is at least 20°C, preferably at least 30°C, often at least 40°C.

In the invention it is preferred that from around 40  
35 to 100 wt% of the total charge is in the form of briquettes. Preferably at least 50 wt%, more preferably at least 70 wt% and most preferably up to 90 or 95 wt% or more

of the total charge is in the form of briquettes. It can be desirable to use a charge which is made up only of briquettes and lime, the lime being included in amounts up to around 10 or 20 wt%.

5       The remainder of the charge can be formed from for instance crushed rock, such as basalt or diabase. Crushed rock is generally provided in a form having a size of at least 50 mm. Preferably 90% by weight of any crushed rock is retained on a sieve of hole size 80 mm. In general at  
10       least 90% by weight of any crushed rock passes through a sieve of hole size 300 mm; preferably at least 90% by weight passes through a sieve of hole size 250 mm; more preferably at least 90% by weight passes through a sieve of hole size 200 mm. In particular it is preferred that any  
15       crushed rock has a size such that at least 90% by weight is retained by a sieve of hole size 80 mm, and at least 90% by weight passes through a sieve of size 160 mm.

Crushed rock is generally present in an amount of 40 wt% or less, based on the total charge, preferably 30 wt%  
20       or less, more preferably 20 wt% or less, most preferably 10 wt% or less.

Raw materials in other forms, for instance finely ground particulate materials, may be included in minor amounts, generally 10 wt% of the charge or less.  
25       Preferably the amount of fine particulate material is substantially zero. Lime can also be included in amounts up to 10 or 20 wt%.

The process of the invention can be used to produce any desired fibre composition.

30       A preferred chemical analysis of the melt, and often of the overall briquette mixture, is as follows, in which all iron is measured as FeO:

	SiO <sub>2</sub>	40 to 65 wt%
	Al <sub>2</sub> O <sub>3</sub>	0 to 6 wt%
35	TiO <sub>2</sub>	0 to 6 wt%
	FeO	2 to 15 wt%
	CaO	5 to 35 wt%

	MgO	2 to 18 wt%
	Na <sub>2</sub> O	0.1 to 12 wt%
	K <sub>2</sub> O	0.1 to 10 wt%
	P <sub>2</sub> O <sub>5</sub>	0.1 to 10 wt%
5	B <sub>2</sub> O <sub>3</sub>	0 to 12 wt%.

Further suitable analyses include those disclosed and exemplified in WO95/29135, WO95/21799, DE 4,417,230, DE 4,427,368, EP-A-495,897, EP-A-558,548 and WO93/22251.

A further suitable analysis for the fibres and  
10 briquettes is as follows, in which all iron is expressed as FeO:

	SiO <sub>2</sub>	32 to 48 wt%
	Al <sub>2</sub> O <sub>3</sub>	10 to 30 wt%, preferably 18 to 30 wt%
	CaO	10 to 30 wt%
15	MgO	2 to 20 wt%
	FeO	2 to 15 wt%
	Na <sub>2</sub> O+K <sub>2</sub> O	0 to 12 wt%, preferably 0 to 10 wt%
	TiO <sub>2</sub>	0 to 6 wt%
	Other Elements	0 to 15 wt%.

20 Suitable analyses include those disclosed and exemplified in the unpublished international applications PCT/EP95/04395.

As explained above, in a briquette mixture of complex chemical analysis various components tend to create  
25 eutectics and contribute to lowered melting points. In particular we find that large amounts of iron and phosphorus together contribute to melting and phase separation, for instance about 3 to about 12 wt% iron and about 3 to about 10 wt% phosphorus. Boron tends to lower  
30 the melting point of briquettes in which it is included, and thus is usually confined predominantly to lower melting point briquettes. We also find that the presence of sodium and other alkali metals often contributes to a low melting eutectic. For instance, more than about 5 wt% alkali metal  
35 together can be problematic. Consequently materials which combine to form a low melting eutectic can be separated into different briquette types. Thus for instance a

briquette type containing a high iron content will generally have a low or zero phosphorus content. Similarly, a briquette having high sodium content may have raised alumina content.

5 We also find that certain compositions result in a low IMT (I) but contain no component which would generally be described as a fluxing agent. Those skilled in the art will be able to formulate briquette types appropriately to achieve the desired values of IMT.

10 Suitable raw materials for forming the briquettes include soda; iron ore; boron-containing materials; phosphorus-containing materials such as apatite; dolomite, quartz sand; olivine sand; mineral wool or other waste material recycled from the manufacture of MMVF; limestone;  
15 rutile; magnesite; magnetite; brucite, bauxite, kaolin, ilmenite, slag material, glass waste material, industrial waste materials, cement or other binder.

Briquettes may be produced in any known and suitable manner.

20 The method of the invention is useful in any type of furnace which can be used to melt raw materials for making MMV fibres. The invention is particularly useful in shaft and cupola furnaces, especially in cupola furnaces, which present a special problem in regulation of melt flow where  
25 low melting materials are used.

The briquettes used in the method of the invention may also be defined in terms of their compression strength across a range of furnace temperatures. Consequently a second aspect of the invention provides a method of making  
30 MMV fibres comprising melting in a furnace raw materials to form a melt and forming fibres from the melt,

in which a proportion of the raw material charge is provided in the form of a mixture of at least two types of briquette (a) and (b) of size at least 50 mm, each type of  
35 briquette having a different chemical analysis, and in which

(1) briquettes (b) have compression strength at each temperature in the range 1,200°C to 1,340°C greater than that of briquettes (a) at the same temperature and at least 30 wt% of the raw material charge is provided by briquettes

5 (b),

and/or (2) the briquettes have an overall chemical analysis which when provided in the form of a single type of briquette gives compression strength (i) which varies across the range of temperatures 1,200°C to 1,340°C, and in  
10 which at least 30 wt% of the raw material charge is provided in the form of briquettes (b) which have a compression strength which is greater than compression strength (i) at each temperature in the range 1,200°C to 1,340°C.

15 The greater compression strength of the briquettes over the defined range of furnace temperatures contributes towards retaining structure within the charge and facilitating the flow, pressure regulation and regular flow of melt. The defined range is the range of temperatures  
20 generally experienced by charge in a furnace, especially a shaft or cupola furnace.

Any of the features discussed above in connection with the first aspect of the invention may be applied to this second aspect of the invention.

25 In the methods of both aspects of the invention the fibres may be formed in any known way. Suitable methods include the spinning cup rotor system and the multiple rotor cascade system.

The products produced in the methods of both aspects  
30 of the invention can be used in any application for which mineral wool is known, for instance as thermal insulation, fire insulation and protection, noise reduction and regulation, growing media, reinforcement of other products, plastics, etc, and as a filler.

35 The invention will now be illustrated with reference to the following examples:

Example 1

Raw materials were provided and melted in a cupola furnace. The melt was formed into fibres using a cascade spinner.

5 The charge comprised the following:

Briquette 1 comprising

	Cement	9.0%
	iron ore	18.0%
	dolomite	2.0%
10	quartz sand	48.0%
	olivine sand	23.0%

Briquette 2 comprising

	Cement	9.0%
	apatite	20.0%
15	quartz sand	37.0%
	olivine sand	22.0%
	dolomite	12.0%.

Briquette 1 (IMT 1200°C) was used in an amount of 37% by weight of the total charge and Briquette 2 (IMT 1240°C) in an amount of 63% by weight of total charge.

20 The IMT (I) of a briquette having the overall briquette composition was 1,215°C.

The fibre making process was without problems and good quality products were produced.

25 In contrast when component (a) was used alone problems in the control of the process arose and good quality products were unobtainable.

Example 2

30 The process of Example 1 was carried out, using the following charge components:

Briquette 1 having the following composition [65% of total charge]:

	Cement	12%
	Ilmenite	4.5%
35	Converter slag	13%
	Quartz sand	45.5%
	Olivine sand	25%

Briquette 2 having the following composition [35% of total charge]:

	Cement	12%
	Apatite	32%
5	Quartz sand	26%
	Converter slag	30%

The IMT of Briquette 1 was 1180°C. The IMT of Briquette 2 was 1240°C.

The IMT (I) of a briquette having the overall  
10 briquette composition was 1,200°C.

Again the fibre making process was without problems and good quality products were produced.

### Example 3

The process of Example 1 was carried out, using the  
15 following charge component:

Briquette 1 having the following composition (50% of the total charge):

	Cement	9%
	Quartz sand	45%
20	Iron silicate	8%
	Sodium borate	20%
	Calcinated soda	18%.

Briquette 2 having the following composition (50% of the total charge):

25	Cement	9%
	Quartz sand	44%
	Olivine sand	20%
	Converter slag	27%.

The IMT of Briquette 1 was 1,000°C. The IMT of  
30 Briquette 2 was 1,260°C. The IMT of a briquette having the overall briquette composition was 1,100°C.

From this charge composition excellent fibres were produced.



**CLAIMS**

1. A method of making MMV fibres comprising melting in a furnace raw materials to produce a mineral melt and forming fibres from the melt,

5 in which the raw material charge includes a mixture of at least two types of briquette (a) and (b), of size at least 50 mm, each type of briquette having a different chemical analysis, and at least 30 wt% of the raw material charge is provided by briquettes (b)

10 and in which

(1) briquette (a) has an initial melting temperature of 1,240°C or below and briquette (b) has an initial melting temperature of 1,200°C or greater and the initial melting temperature of briquette (b) is at least 20°C  
15 greater than the initial melting temperature of briquette (a),

or

(2) the briquettes have an overall chemical analysis which when provided in the form of a single type of  
20 briquette gives an initial melting temperature (I), and in which briquettes (b) have an initial melting temperature which is at least 20°C greater than initial melting temperature (I).

2. A method according to claim 1 in which 70 to 90 wt% of  
25 the raw materials are provided in the form of briquettes.

3. A method according to claim 1 in which initial melting temperature (I) is 1,200°C or below.

4. A method according to any preceding claim in which the mixture comprises only two types of briquette.

30 5. A method according to any preceding claim in which substantially all of the briquettes have initial melting temperature at least 20°C above initial melting temperature (I).

6. A method according to any preceding claim in which the  
35 overall chemical analysis of the briquette mixture comprises iron in an amount of from 3 to 12 wt% and phosphorus in an amount of from 3 to 10 wt%.

7. A method according to any preceding claim in which the overall chemical analysis of the briquette mixture comprises alkali metal in an amount of 5 wt% or more.

8. A method according to any preceding claim in which the  
5 furnace is a shaft or cupola furnace, preferably a cupola furnace.

9. A method of making MMV fibres comprising melting in a furnace raw materials to form a melt and forming fibres from the melt,

10 in which a proportion of the raw material charge is provided in the form of a mixture of at least two types of briquette (a) and (b) of size at least 50 mm, each type of briquette having a different chemical analysis, and in which

15 (1) briquettes (b) have compression strength at each temperature in the range 1,200°C to 1,340°C greater than that of briquettes (a) at the same temperature and at least 30 wt% of the raw material charge is provided by briquettes (b),

20 or (2) the briquettes have an overall chemical analysis which when provided in the form of a single type of briquette gives compression strength (i) which varies across the range of temperatures 1,200°C to 1,340°C, and in which at least 30 wt% of the raw material charge is  
25 provided in the form of briquettes (b) which have a compression strength which is greater than compression strength (i) at each temperature in the range 1,200°C to 1,340°C.

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 C03C13/00 C03C1/02 C03B3/00 C03B5/16

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 C03C C03B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	GB,A,2 027 690 (CENTRAL GLASS COMPANY) 27 February 1980 see abstract ---	1-5
Y	US,A,4 969 940 (C. H. SCHWARB ET AL.) 13 November 1990 see abstract ---	1-5
A	WO,A,92 04289 (PAROC OY AB) 19 March 1992 see example ---	1-8,10
A	FR,A,2 690 438 (ISOVER SAINT GOBAIN) 29 October 1993 see page 1, line 16 - page 2, line 19 ---	1-8,10
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☒ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

## \* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
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Date of the actual completion of the international search

8 July 1996

Date of mailing of the international search report

22.07.96

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Reedijk, A

## INTERNATIONAL SEARCH REPORT

International Application No

PCT/EP 96/01063

## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	PATENT ABSTRACTS OF JAPAN vol. 13, no. 487 (C-649) [3835] , 6 November 1989 & JP,A,01 192743 (NIPPON STEEL CHEM CO LTD), 2 August 1989, see abstract	1-8,10
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Information on patent family members

International Application No

PCT/EP 96/01063

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